

METHOD AND APPARATUS FOR RAPID TOMOGRAPHIC MEASUREMENTS OF
THE ELECTRICAL CONDUCTIVITY DISTRIBUTION OF A SAMPLE

SPECIFICATION

FIELD OF THE INVENTION

5 Our present invention relates to a method and apparatus
for the rapid tomographic measurement of the electrical
conductivity distribution in a sample.

BACKGROUND OF THE INVENTION

10 Reference to tomographic measurements of electrical
conductivity distribution in a sample are intended to mean that
the conductivity distribution of a sample, which can be a ground
sample, aquifer sample, other geological sample, but also
biological materials and the like in turn of the various cross
sections through the sample.

15 For understanding of practically all significant
questions in conjunction with heterogeneously structured samples,
a knowledge of the spatial structure of the sample is of
paramount significance. In the case of a heterogeneously
structured sample, for example ground, aquifers and other

geological samples, this knowledge has required above all
invasive processes, for example, test drilling. Such invasive
processes have the drawback that they alter the conditions in the
sample. Furthermore, the determination of the structure only
5 takes place at selected points in the sample. Important
relationships can remain undiscovered and this applies in
particular to transport processes in subterranean strata.

More recently, less intensive geophysical and
geoelectrical methods have been developed for geological
10 investigations. It is possible, for example, to measure a
variety of geological parameters by noninvasive methods or
methods which are less invasive, utilizing sensors which can be
forced into the ground or are provided in the region of the
ground and which measure geological parameters directly or
15 measure parameters which can be interpreted in turn by biological
structures.

For example, a geoelectric method is known whereby at
least two electrodes are inserted into the ground and a voltage
measuring unit is connected with the electrodes so that the
20 electrical potential distribution can be measured and from that
distribution the electrical conductivity distribution can be
determined.

Another method known to the art, namely, controlled source audiomagnetotelluric (CSAMT) provides one or more electrical dipoles in the ground which are driven in the frequency range of 1 Hz to 8 kHz at a relatively large distance from such a dipole (often several kilometers) a magnetic and electrical component of the radiated electromagnetic waves are measured. With this process geological structures can be determined at a considerable depth and distance.

A geoelectromagnetic method is likewise known whereby the ground is excited with coils on the ground surface or by means of a transmitter spaced therefrom and a magnetic field induced subterraneously by reaction with external magnetic field is measured.

From DE 198 37 828, a method of calculating a current density distribution in a subterranean sample is known in which two electrodes are implanted in the ground sample. A low-frequency electrical alternating current is supplied to the electrode and a current density distribution of this current is effected in the subterranean sample as a function of the conductivity distribution therein. This results in a magnetic field intensity distribution which can be measured with the aid of a magnetic field sensor. From the magnetic field distribution

the current density distribution can be calculated. This in turn allows the conductivity distribution in the subterranean sample to be determined. The conductivity of the sample is the target value and allows properties of the sample to be determined. DE 5 198 37 828 also discloses an apparatus for carrying out that method using a lock-in amplifier evaluating the measured signal.

As a general matter, in conductometry the measurement of the voltage drop or the potential difference in a sample to be investigated is a prerequisite for calculating the conductivity 10 of the sample. For this purpose, the sample can be supplied for example with alternating current. From the measured potential differences and the amplitude of the current measured in the conductors supplying that alternating current, the specific electrical resistance and its converse, the conductivity of the 15 sample, can be calculated. In cases in which the magnetic field strength distribution is to be measured, the conductivity of the sample can be calculated as well from the measured current amplitude and the magnetic field strength.

In geoelectric measurements the multidimensional 20 conductivity distribution in samples can be determined for example by the application of current and the measurement of potential differences. For this purpose, the sample is usually

contacted with a large number of electrodes. An alternating current is preferably launched into the sample by each two electrodes of this array of electrodes, for example into the ground. Each application of alternating current generates an associated electric potential distribution as a function of the electrical conductivity distribution in the sample. At other electrodes the potential difference is measured.

From the measured electrical potential and/or the measured magnetic field for a sufficiently large number of different applications of electrical excitation signals, the conductivity distribution in the sample can be calculated by means of special calculating techniques. The method of application of current and measurement of electrical or magnetic fields is used in many geophysical investigations with different electrode arrangements, like, for example, the Schlumberger sounding, Wenner mapping, dipole-dipole arrangements, four-point measurements in two-dimensional or three-dimensional tomography (electrical resistivity tomography: ERT) with flat or round electrode elements.

A drawback of earlier measurement systems and methods is that the current supply requires energization of respective pairs of electrodes of the entire set. The total measurement

time thus corresponds to the sum of the individual measurements for an excitation. The total measurement time is a function of the measurement arrangement and the desired resolution and precision and thus can be very long. When for example an
5 individual measurement for a particular precision requires a measurement time of 30 minutes, the total measurement time for 10 excitations can consume 5 hours. In samples in which the conductivity distribution is the targeted parameter and the measurement should be carried out in a shorter period of time,
10 the measurement devices of the prior art have not been found to be suitable.

In Cheney et al (Cheney, M., Isaacson, D., Newell, J.D., 1999. Electrical impedance tomography. SIAM Review, Vol. 41. pp 85-101) a method of electrical impedance tomography has
15 been described in which the electrical conductivity measurement of a human body utilizes the application of electric currents independently from one another and in succession. A drawback of this system is that the measurement device is only suitable for samples like those of the human body. More complex samples, for
20 example, geophysical samples, cannot be characterized by such systems or are characterizable only limitedly by them.

OBJECTS OF THE INVENTION

It is, therefore, the principal object of the present invention to provide a noninvasive method for the rapid tomographic measurement of conductivity distribution in a sample with high resolution, especially for the variation of the conductivity distribution with time.

Another object of the invention is to provide an improved apparatus for a rapid tomographic evaluation of a complex sample like a geophysical sample.

Still another object of the invention is to provide a method of and an apparatus for the rapid tomographic measurements of a conductivity distribution whereby drawbacks of prior art systems are avoided.

SUMMARY OF THE INVENTION

These objects and others which will become apparent hereinafter are attained, in accordance with the invention, in a method for the rapid tomographic measurement of conductivity distribution in a sample which comprises the steps of:

(a) launching electrical excitation signals simultaneously into a sample from a multiplicity of locations distributed in the sample;

(b) measuring at a multiplicity of locations in the sample at least one parameter selected from the group which consists of potential difference and magnetic field strength resulting from the electrical excitation signals; and

5 c) correlating the measured potential differences or magnetic field strengths with the launched excitation signals to provide conductivity distribution cross section in same sample.

A method can be carried out, according to the invention with an apparatus which comprises:

10 an electrical excitation source coupled with the sample for applying electrical excitation signals thereto;

 at least one device coupled with the sample for measuring a potential difference or magnetic field strength therein in proportion to the electrical excitation signals

15 supplied thereto; and

 circuitry for correlating measured potential difference or magnetic field strength proportionally with the supplied electrical excitation signals.

 The method of the invention thus applies a multiplicity
20 of electrical excitation signals simultaneously to the sample to be explored and a correlation of the measured signals (potential

differences and/or magnetic field strength) proportional to the fed electrical excitation signals is carried out.

5 The advantage of the method of the invention is primarily to be found in the substantial measurement time which is required by comparison to the measurement methods involved sequential applications of the electrical excitation signal as required by the art. This means that by contrast with n sequential applications of an excitation signal to respective pairs of electrodes as is known in the art, with the method of
10 the invention only a single application of n excitation signals to a multiplicity of spaced-apart excitation electrodes is effected in parallel. The measurement time is reduced by a factor n to $1/n$ of the prior art measurement duration. This enables a better evaluation of the sample at a particular time,
15 especially when the conductivity distribution in a sample may not have reached a steady state. This is especially the case in flow processes. The method is for the most part noninvasive since the insertion of the electrode at the multiplicity of locations can be done without significant disturbance of the sample, especially
20 in the case of geological samples.

 According to a feature of the invention, the electrical excitation signals launched in the sample are applied to the

latter as orthogonal signals. Two signals are orthogonal to one another and thus mutually independent when the scalar product of the orthogonal signals written in vector form is zero. The requirement herein that orthogonal excitation signals be applied is, however, not a requirement that only two mutually orthogonal excitation signals be applied at each excitation point. In other words, usually the method of the invention will apply the excitation from a multiplicity of electrodes simultaneously in a sample to be investigated. Each excitation produces an associated current density distribution as a function of the electrical conductivity distribution. The different signals are applied by means of electrodes at the respective locations and by energization of these electrodes at the respective positions by appropriate circuitry. The resulting potential field distribution and/or magnetic distribution measured in each case will be the sum of all of the orthogonal excitation signals over a particular region. Each measurement, therefore, is not restricted to two mutually orthogonal excitation signals.

The measured potential and/or magnetic field strength distributions can be broken down based upon the orthogonality of the excitation signal in accordance with the proportion from each excitation signal and thus the relationship of the current

density distribution to that excitation signal can be determined. The application of orthogonal signals thus serves as a means whereby a multiplicity of electrical excitation signals can be supplied at different launching positions simultaneously to enable different current density distributions to be created in the sample and resulting measurement signals to be separated and associated with them.

As a consequence it is possible for the measured electromagnetic distributions of potential differences and/or magnetic field strengths, to be broken down and associated with the excitation signals and thus coordinated with them.

The rapid investigation of complex three-dimensional samples like ground samples, aquifers and other biophysical samples can be undertaken in a rapid tomographic manner.

The electrical excitation signal can advantageously be orthogonal sinusoidal signals which are applied to the sample via electrodes. The individual signals can be of the type analyzable with a cosine series, sine series or Fourier series.

From the measured signal, for example corresponding to a term in the resulting Fourier series, the defining equation for the Fourier coefficients can be easily calculated.

In accordance with a further feature of the invention for the orthogonal sinusoidal signals, only the individual terms of the cosine series can be fed to the sample and the measured signals separated into the cosine portion of a Fourier series by
5 a means-defining equation for the Fourier coefficients. This provides an especially simple method for determining the real part of the electrical conductivity distribution.

An additional separation of the signal to obtain the sine component (imaginary part) of the Fourier series enables the
10 distribution of the complex electrical conductivity to be determined for the sample. A method of this type is interesting especially for investigation of such samples which show a phase shift between the current and variety because of induced polarization effects. In this case, in addition to the cosine
15 component, the Fourier coefficients of the sine part can be calculated. This method supplies a greater amount of information with respect to the material of the sample since it takes into consideration both electrical conductivity and polarization phenomena. The method forms the basis for an electrical
20 impedance tomography independently of whether the potential differences or magnetic field strengths are measured.

Instead of continuous orthogonal sinusoidal scans, simple orthogonal coding binary signals can be used which can assume only two possible amplitudes, for example +1 and -1. A single bit sequence is then so coded with the individual sequences (vectors) are orthogonal to one another. In this manner a simultaneous application of the excitation signal and a decomposition of the measured signal into respective components relating to the excitation signals is possible. These binary signals can contribute to a further simplification since it is only necessary to time the switch between two states. The computer costs for decomposing the signals into orthogonal components is less and it is, of course, much simpler to carry out the method of the invention.

The rapid measurement of potential differences, according to another feature of the invention, utilizes at least three electrodes for excitation of the sample. Then at least two additional electrodes can be used for measurement of the potential distribution by being inserted into the sample. As a consequence, electrical excitation signals are applied simultaneously with measurement of the potential distribution.

Electrical excitation signals can be simultaneously applied to at least a part of the excitation electrodes so as to

obtain in a targeted manner for each excitation signal an associated characteristic current density distribution in the sample, whereby potential differences are obtained in the sample as a function of the conductivity distribution. These values are
5 determined as a function of the positions of the electrodes in the sample in proportion to the voltage.

From the measured potential differences and the electrical excitation signals, and the current amplitude, the specific electrical resistance or its inverse conductivity
10 distribution in the sample can be calculated as target parameters. The excitation signals and the measurement of the potential differences can be carried out using the same electrodes, at least in part. In this case, the excitation signals may be electric current from a high ohmic current source.
15 The interfacial resistance between electrodes and the sample are taken into consideration in the later calculation of the resistance distribution. In a preferred embodiment, electrodes in the form of electrode spikes are provided which have electrode surfaces which are electrically decoupled from one another, one
20 surface of each electrode being utilized to feed the electrical excitation signal while another is used to measure the potential.

The use of a single electrode for applying the excitation signal and for measuring the potential keeps the cost of the apparatus for producing the method relatively low. The electrode spikes can have a tip of solid metal forming the potential measuring
5 portion separated by an annular insulator from a metal jacket or tube forming the portion for applying the excitation voltage.

The method need not be used exclusively for tomographic measurement of potential differences but can also be employed for rapid measurement of magnetic field strength in the sample.

10 Preferably both potential differences and magnetic field strengths can be measured.

In accordance with the invention at least three electrodes in spaced-apart relationship in the sample are used for feeding the electrical excitation signals into the sample.

15 At least one magnetic field sensor is then provided in or adjacent the sample for measuring of a resultant magnetic field strength distribution at the surface, within the sample or outside the sample.

20 Simultaneously electrical signals are supplied to the sample from at least a portion of at least three electrodes with the goal of producing for each excitation signal an independent current density distribution in the sample. As a result, within

the sample there arises independently of the conductivity distribution a current density distribution which is superimposed for all signals and which produces a magnetic field distribution which can be measured by the magnetic field sensor or sensors at
5 selected spaced-apart points.

The correlation of the measured magnetic field intensity distribution in proportion to the applied electrical excitation signal can allow the respective magnetic field distribution for each current distribution to be determined.

10 From the known electrical signal strength at the excitation electrode, e.g. as measured in terms of the current through the respective electrode and the measured magnetic strength, the conductivity distribution can be calculated.

In spite of or in addition electrodes for excitation of
15 the sample at least two coils can be used to increase the flexibility of the method.

It is especially advantageous, therefore, to measure both potential differences and magnetic field strengths. It is thus possible, within the scope of the present invention, to
20 provide coils as well as electrodes for applying the excitation in the form of electrical or electromagnetic signals and for measuring the potential differences and/or magnetic field

strengths which arise, e.g. through the use of further electrodes and/or magnetic field sensors. From these results the complex conductivity distribution of the sample can be calculated. With simultaneous measurement of potential differences and magnetic field strengths, the spatial resolution of the conductivity distribution in the sample can be significantly raised. In this case in addition to the electrodes for measuring the potential differences, at least one and preferably a plurality of magnetic field sensors can also be used to determine the magnetic field strength distribution.

It is advantageous to launch the electric signals as alternating current or alternating voltages into the sample. This can be done in a simple manner utilizing for example alternating current or alternating voltage generators. Independently of the method of calculation to determine the conductivity distribution, the current or voltage which is applied as the excitation signal can be measured at or in circuit with the electrodes insofar as these values are not known.

It is also possible, in accordance with the invention not to use the advantage of a shortened measuring time but rather to carry out the method with a sequential excitation of the sample. In this case, the statistical precision of the

measurements for a given electrical excitation energy per
excitation signal can be significantly better or one can achieve
the same statistical precision as with a lesser amount of
excitation energy per excitation signal. In the latter case, the
5 excitation signals per electrode can be selected to be
significantly weaker as a greater number of electrodes are
provided. This is especially important for measurements in
samples which are highly nonlinear since in those cases, unlike
media with linear qualities, a reduced current per electrode can
10 provide better tomographic imaging.

An apparatus for the rapid measurement of conductivity
distribution in a sample can comprise a first means for applying
an electrical excitation signal to the sample and a second means
for measuring the resulting potential differences and/or magnetic
15 field strengths. The apparatus can comprise yet further means
for simultaneous application of the electrical excitation signals
to the sample as well as means for separating the measurement
signals, i.e. decomposing them, so that a correlation of the
measured potential differences and/or magnetic field strengths in
20 proportion to the applied electrical excitation signal is
possible and thus the respective current distribution can be
determined.

Furthermore it is advantageous to synchronize the means for generating the excitation signal and means for acquiring the measured signal in a temporal manner. That ensures that tomographic measurements of the multidimensional complex conductivity distribution in a sample can be effected rapidly. In addition, the separation of the measured signals into orthogonal signals is facilitated.

The means for feeding electrical signals into the sample can comprise electrodes and/or coils.

The means for measuring the resulting potential difference and/or magnetic field strength, in turn, can be electrodes and/or magnetic field sensors.

The apparatus can also comprise a control unit, e.g. a computer which can form the means for simultaneously applying the electrical excitation signal to the electrodes and/or coils in the sample and for acquiring the measured signal and/or decomposing them into the respective components to effect the correlation previously described. This computer-controlled unit can produce mutually orthogonal electrical excitation signals and enable the separation of the measured potential differences and/or magnetic field strength proportionally to the fed electrical signals.

The apparatus can generate the orthogonal signals (sinusoidal signals or orthogonal coded signals) and apply them to the electrodes or coils.

5 The apparatus for example can have at least two generators forming part of the control and computer unit for producing orthogonal electrical signals. Conductors between the electrodes and the generators serve to deliver the electrical signal for excitation purposes to the sample.

10 A separating stage can be provided as part of the control and computer units to break down the measured signals (potential differences and/or magnetic field strengths) in proportion to the excitation signals fed to the sample and enable the correlation.

15 The apparatus also includes, advantageously an evaluating unit or stage for calculating the conductivity distribution from the measured potential differences and/or the measured magnetic field strength as well as the known data for the excitation signals (current amplitudes and/or voltages).

20 To feed the electrical excitation signals into the sample, at least three electrodes can be provided. The more electrodes which are used for independent application of

excitation signals, the better will be the spatial resolution of the tomographic measurements in the sample.

The second means for measuring the potential difference should comprise at least two electrodes. Again, when a greater
5 number of electrodes are provided for measurement of the potential difference, the more precise will be the measurement and hence the tomographic analysis.

According to a feature of the invention, therefore, the first means for exciting the sample can have at least three
10 electrodes which can be in the form of electrode spikes and which are driven into the sample, usually a geological sample. The spikes may have, in addition, surfaces for measuring the potential difference. By comparison with earlier systems, an arrangement in which the spike, according to the invention,
15 serves both for applying the excitation signal to the sample and for measuring the potential difference, affords a considerable saving in the number of electrodes which are used. The metal tips of the spikes can serve as the electrodes for potential measurement while the jackets of the spikes form the excitation
20 electrodes. The jackets and tips are electrically separated from one another. Electrode spikes of this type can be driven into relatively dense samples like ground samples and aquifer samples.

Installation of such electrodes in the sample can be carried out in less than half the time previously required for placing electrodes in a sample at least in part because a single spike can serve both for excitation and measurement. The placing of
5 the electrodes can simplify and speed up the investigations of relatively complex ground samples as a result.

Instead of or in addition to the electrodes, at least two coils can be placed in or adjacent the sample for applying a magnetic field thereto. The coils induce primary magnetic fields
10 which can result in eddy currents within the sample and the resulting overall magnetic activity can be registered by means of at least one magnetic field sensor. Electrodes can also serve to measure potential differences arising from the eddy currents in the sample.

15 The apparatus according to the invention can thus include at least two electrodes, in addition to those used for excitation, for measuring the potential difference and at least one magnetic field sensor for the simultaneous measurement of a magnetic field strength. This combination affords excellent
20 resolution with respect to conductivity distribution determinations.

BRIEF DESCRIPTION OF THE DRAWING

The above and other objects, features, and advantages
5 will become more readily apparent from the following description,
reference being made to the accompanying drawing in which:

FIG. 1 is a highly schematic illustration of an
apparatus for tomographic conductivity determination in a sample;

FIG. 2 is a diagram of another apparatus in accordance
10 with the invention;

FIG. 3 shows the excitation of a sample with a
multiplicity of generators so that orthogonal signals are
produced;

FIG. 4 shows still another apparatus in accordance with
15 the invention; and

FIG. 5 is a diagram similar to FIG. 1 but illustrating
another aspect of the invention.

SPECIFIC DESCRIPTION

FIG. 1 shows in highly schematic manner an application
20 of the invention in which geoelectric resistance soundings are
taken in accordance with the Schlumberger principle, modified in

accordance with the invention. An electrode pair consisting of electrodes E and F serves for the measurement of a potential difference U_0 while two further electrode pairs A and B as well as C and D serve to launch alternating current signals I1 and I2 into the ground structure in which the electrodes are inserted. The latter forms the sample S which is below grade G. The current signals I1 and I2 are time-continuous, orthogonal sinusoidal signals

$$I_i = c_i \cos(i\omega_0 t)$$

where C_i is a peak value of the excitation alternating current amplitude and t is time, i being the number of signals 1 and 2 and ω_0 is the base frequency $\omega_0 = 2\pi f_0$.

The signals correspond to the cosine term of a Fourier series and are orthogonal since the prerequisite for orthogonal signals is

$$\int_0^T I_i(t) I_k(t) dt = 0 \text{ for } i \neq k$$

where $i = 1 \text{ or } 2, k = 1 \text{ or } 2$.

In this example, only the first two terms are selected.

The sinusoidal excitation signals have the frequencies $1\omega_0$ and $2\omega_0$. The integration time T is, as a rule, the duration of a period $1/f_0$ or a multiple of $1/f_0$. Because of the excitation with the independent currents I_1 and I_2 , two geometrically different current density distributions j_1 and j_2 arise in the subterranean sample. For low excitation frequencies and a real value specific resistance distribution in the sample, the measured potential difference is given by

$$U_G = \sum_i a_i \cos(i\omega_0 t) = \sum_i U_i \quad (1)$$

with $i = 1$ and 2 , a_i is the peak value of the proportional measured voltage amplitude and ω_0 is the base frequency of the excitation signals launched into the sample.

The measured potential differences are derived from the cosine terms of the Fourier series and can be decomposed into the individual voltage components U_i (or potential differences) with the frequencies $1\omega_0$ and $2\omega_0$ which are generated by the currents I_1 and I_2 . The peak values a_i are the real coefficients of the

Fourier series and are determined by the defining equations for the Fourier coefficients:

$$a_i = \frac{2}{T} \int_0^T U_G(t) \cos(i\omega_0 t) dt$$

For the proportional potential differences

5

$$U_i = a_i \cos(i\omega_0 t)$$

applies.

From the known excitation current I_i , the voltage U_i and the known geometric positions of the electrodes, the conductivity distribution in the sample can be determined. The resolution increases with the number of measuring electrodes and with the number of geometrically different current density distributions in the samples which are produced by means of the orthogonal excitation current.

For samples which generate a phase shift between current and voltage, an expansion of equation (1) is required. The measured phase-shifted voltage U_e

$$U_G = \sum_i a_i \cos(i\omega_0 t) + b_i \sin(i\omega_0 t) = \sum_i U_i$$

is determined by the voltage components U_i together. The additional coefficients b_i are also determined by the defining equation for the Fourier coefficients (in this case, the sine components):

$$b_i = \frac{2}{T} \int_0^T U_G(t) \sin(i\omega_0 t) dt \quad i=[1,2]$$

The partial voltages with which the respective excitation currents are associated are thus:

$$U_i = a_i \cos(i\omega_0 t) + b_i \sin(i\omega_0 t).$$

The phase shift ($-\arctan(b_i/a_i)$) and the amplitude $\sqrt{(a_i^2 + b_i^2)}$ of partial voltages U_i phase shifted relative to the currents I_i are thus known.

The latter analysis also supplies the amplitudes of the partial voltages U_i when the exact phases of the excitation signals are not known. This is especially important when no separating stage synchronization generator is used, since they generate a sinusoidal signal with unknown phase position. For

simple resistance tomography no synchronizing generators are required in accordance with this method. When one starts with real specific resistances of the sample, the phase shift can only stem from nonsynchronized generators and is thus without
 5 significance.

The number of the current I_1 is, as in this example, not limited to two, but can be optionally increased. By way of example, with a base frequency f_0 of 0.1 Hz in a frequency range of 10 Hz to 19.9 Hz, 1000 orthogonal signals can be accommodated.
 10 The minimum measurement time in this case was $1/f_0 = 10$ seconds. One should, however, choose a time window T in the steady-state of the system so that the measurement as a rule is lengthened by the transient time.

Instead of a time-continuous sinusoidal excitation
 15 signal, we can use discrete-time signals

$$I_{i,n} = c_i \cos(i\omega_0 n T_a) \quad I = [1, 2]$$

with the scanning time T_a and the number n of the scanning value in the range 1 to N . The latter can be generated and processed simply by means of digital data processing. The currents I_1 and
 20 I_2 in this case are orthogonal vectors with respective N values. The number N is so chosen that $N \cdot T_a = 1/f_0$ or a multiple of $1/f_0$.

In the practical application, the excitation currents are generated locally or centrally and applied to the electrodes and are phase-synchronized with respect to one another and to the separating stage T by the control and computing unit S so that the mathematically required operations corresponding to the above-mentioned equations can be correctly carried out in the unit S. The unit S encompasses at least two generators for producing orthogonal signals. They can be quartz-controlled sine wave generators whose frequencies can be adjusted in accordance with the foregoing example. The signals can, as necessary, be further amplified by power amplifiers with current or voltage outputs.

Even better is an excitation generator in which the orthogonal signals (for example cosine signals with frequencies $i \cdot f_0$) are calculated by a PC or some other computer unit and are simultaneously outputted over a corresponding number of DAC (digital-analog-converter) channels and respective power amplifiers.

In the case of orthogonal coded signals, the DACs and the power amplifier(s) can be replaced by simple power switches which switch between two levels. This affords a further simplification.

The separating stage T, which serves to separate the measured signals and which is contained in the unit S, is comprised in the simplest case of an ADC (analog-digital-converter) which digitalizes the signals, and a computing unit which decomposes the signals into components associated with the respective excitation signals.

The computer in the unit S can be realized as a PC, a microcontroller, microprocessor, digital signal processor or other programmable component capable of fulfilling the indicated requirements. An analog computer or computing unit is also possible.

This example is applicable to determinations of specific resistance in resistance depth soundings according to Schlumberger in subterranean samples at different depth regions simultaneously.

The method is not, however, limited only to geoelectric measurements, but can be used for all investigations for which previously a sequential application of current sources or voltage sources was provided.

A further example has been illustrated in FIG. 2. This arrangement, shown in highly schematic form, constitutes a device for rapid tomographic investigation of the conductivity

characteristics in heterogeneous samples, here a lysimeter. The lysimeter L is shown as a cylinder in plan view. In addition to electrodes illustrated in FIG. 1, in this embodiment two further electrodes G and H have been provided for measuring the potential difference.

The alternating currents or alternating voltages re generated in the modules M1 to M4. These modules are controlled by PCs or microprocessors. The separation of the measured signals is effected either in the modules or in the PC. The arrangement of the electrode corresponds to that in a typical electrical resistance tomographic application (ERT). For each electrode, the resistance between the electrode and the ground must be constituted in calculating the conductivity subsequently. Current sources are preferred for the excitation signal.

In a further embodiment of the invention, instead of the electrode pairs C-G, H-D A-E and B-F, four electrode spikes can be used for feeding the electrode excitation signal to the sample and can have two electrically decoupled surfaces for the simultaneous potential measurement (see the concurrently copending application Ser. No. _____ (Attorney's docket No. 22623) corresponding to German application 102 38 823.7 filed 23 August 2002.

In addition to the potential differences or instead of a potential difference measurement, the magnetic field can be measured. In FIG. 2 the magnetic field sensors have been indicated at I, J, K and N. This arrangement can also be used for exploring neighboring surfaces of the ground by corresponding geoelectric and/or geomagnetic methods.

Of course the number of electrodes used can be increased as required to obtain a higher resolution. Thus the number electrodes shown in FIG. 2 should be considered only exemplary.

In general the method of measuring the spatial distribution of electromagnetic fields like potential distributions and magnetic field strength distributions can be applicable to any kind of sample to which electrical signals can be effectively applied. From the measured potential differences and/or magnetic field strengths and known strengths of the alternating current which are fed to the samples, specific resistances or conductivity distribution in the sample can be calculated.

FIG. 3 shows an arrangement corresponding to FIG. 4 with four excitation electrodes. The sample is a square body. Instead of the potential measurement with the electrodes E-F as

in FIG. 1. In FIG. 3 the magnetic field is measured with a magnetic sensor E' and converted into a voltage U_0 . This voltage is fed to an analog to digital converter ADC and then supplied to the separating stage T and decomposed to the components U_1-U_6 corresponding to the respective excitation currents.

In this system, in addition to the two currents I_1 and I_2 , four further currents I_3 to I_6 are generated and applied. With four excitation electrodes and current feed to respective electrode pairs, a maximum of six geometrically different current density distributions can be produced in the sample by means of six mutually orthogonal excitation currents. In this embodiment, therefore, all possible combinations of the current fed to the respective pairs of electrodes (AB, AC, AD, BC, BD, CD) are used.

FIG. 4 shows an arrangement similar to that of FIG. 3. Here, however, instead of six excitation currents I_1 to I_6 , four excitation voltages Q_1 to Q_4 are generated and applied to the electrodes A, B, C, D. With four excitation electrodes and voltage feeds, a maximum number of the independent current density distributions can be produced in the sample utilizing four mutually orthogonal excitation voltages. In this case, the pickup E' provides the signal U_0 of the analog digital converter

ADC and the separator T from which four voltage components Q_1 to Q_4 corresponding to the excitation voltages are obtained.

In FIG. 5, instead of orthogonal continuous sinusoidal signals, simple binary orthogonal coded signals are used which can assume only amplitudes $+C$ and $-C$. To the electrode pairs A and B and C and D, the values of the alternating voltages (Q_1 and Q_2) are applied where, for example,

$$Q_i = c S_i,$$

where $i = 1, 2$ and

$$S_1 = (-1, +1, +1, -1),$$

$$S_2 = (+1, +1, -1, -1).$$

The signals are applied in succession in this order. The Signals S_1 and S_2 are orthogonal to one another since the potentials at the electrodes B and D are always equal to this scale of product of S_1 and S_2 is zero.

$$S_i S_k^T = 0 \text{ for } i \neq k,$$

with $i = 1$ or 2 ,

with $k = 1$ or 2 .

Thus Q_1 and Q_2 are also orthogonal to one another.

Based on the feed with independent voltages Q_1 and Q_2 , in the subterranean sample two independent current density distributions j_1 and j_2 develop in the subterranean sample. For low excitation

frequencies and real specific resistance of the sample, the measured potential difference is:

$$U_G = \sum_i a_i S_i = \sum_i U_i$$

with $i = 1$ and 2 ,

a_i = measurement voltage amplitude.

The measured potential difference collects the signals S_i . The real coefficients a_i are determined by means of the scalar products from U_G and S_i in accordance with the following equation:

$$a_i = (U_G S_i^T) / N$$

where N is the number of the value of each vector.

In this example, $N = 4$. For the potential difference the following apply:

$$U_i = a_i S_i.$$

The excitation currents $I_{AB,G}$ and $I_{CD,G}$ which flow the electrode pair are measured and decomposed into components $I_{AB,i}$ and $I_{CD,i}$, based upon

$$I_{AB,i} = b_{AB,i} S_i \text{ with } b_{AB,i} = (I_{AB,G} S_i^T) / N, \text{ and}$$

$$I_{AB,i} = b_{AB,i} S_i \text{ with } b_{AB,i} = (I_{AB,G} S_i^T) / N,$$

from the determined excitation current components, the voltages U_i and the known geometric positions of the electrodes, the specific resistance distribution in the sample can be determined. In this example the resolution as to location can be enhanced by the use of further excitation electrodes, orthogonal current feeds and measurement sensors.

The invention is applicable , *inter alia*, to the following fields in geophysics:

Determination of the concentration of soluble substances in the ground and in ground water aquifers by the determination of conductivity distributions in accordance with the invention.

Observation of chemical processes by measurements of the variation in space and time of the conductivity distribution (for example precipitation reactions).

Trace analysis and investigation of electrical anomalies (to determine the presence or absence of metallic bodies, ores, conductors, archeological objects and the like.

Detection and monitoring of preferred flow and transport paths in porous media (for example the ground, aquifers, rock structures, lysimeters.

Deposits of agrochemicals.

Catastrophe management in the case of industrial accidents.

Protection and environmental determination in industrial sites.

Monitoring of laboratory and agricultural facilities with respect to transport in porous media.

Determination of particle and colloid transport.

Investigations with respect to poorly conducting liquids in the ground in ground water, including development of water films on granular material and the location and distribution of contaminants like oil or contaminating organics, the sanitation of soil and the monitoring of waste dump for leakage.

Monitoring of dikes for leakage.

The exploration for water carrying or water guiding layers in arid or semiarid environments.

The monitoring of salt water/sweet water in subterranean systems including aquifers and agronomy.

The following fields of use in medicine are also applications of the invention:

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Clinical monitoring for respiratory function,
determination of lung and heart functions and *in vivo*
investigations into impedance distribution in the thorax.

Basically the method and apparatus of the invention can
also be used for material testing.